

SPECIFICATION

RUBBER COMPOSITION AND TIRE USING THE SAME

TECHNICAL FIELD

[0001] This invention relates to a rubber composition and a tire using the same, and more particularly to a rubber composition for a tire tread having a high wear resistance and a low heat buildup.

5 BACKGROUND ART

[0002] Heretofore, a carbon black is compounded into rubber as a filler, and the rubber is reinforced by the compounding of the carbon black to improve physical properties of rubber such as wear resistance, tensile strength and the like. In general, a carbon black having a high reinforcing property can be obtained by controlling a surface nature of the carbon black, but a light transmittance of toluene extract is lowered at the same time to increase a tar component adhered onto the surface of the carbon black and hence this tar component obstructs the reinforcing property inherent to the carbon black. Therefore, there is naturally a limit for improving the reinforcing property of the carbon black (see JP-A-2000-53883, JP-A-10-36703 and JP-A-9-40883).

[0003] Also, rubber compositions compounded with the carbon black having a high reinforcing property are excellent in the wear resistance and the like, so that they are suitable as a tread rubber for a tire. In recent years, however, the rubber composition used in the tread rubber is required to be excellent in the low heat buildup in addition to the wear resistance from a demand of reducing a fuel consumption of the tire. These two performances are usually conflicting with each other, so that the establishment thereof is made first possible by improving the filler such as carbon black or the like.

DISCLOSURE OF THE INVENTION

[0004] It is, therefore, an object of the invention to solve the problems of the conventional technique and to provide a rubber composition possessing a high wear resistance and a low heat buildup.

30 Also, it is another object of the invention to provide a tire having

excellent wear resistance and low heat buildup in which the above rubber composition is applied to a tread.

[0005] The inventors have made various studies for achieving the above objects and found that when a diene polymer is compounded 5 with a carbon black to form a rubber composition, the diene polymer is highly reinforced by using a carbon black being less in a tar component existing on its surface, particularly polycyclic aromatic component, whereby high fracture strength and wear resistance are obtained in the rubber composition and further heat buildup of the rubber composition 10 is suppressed to a low level, and as a result, the invention has been accomplished.

[0006] That is, the rubber composition according to the invention is a rubber composition comprising 100 parts by mass of a diene polymer and 20-250 parts by mass of a carbon black as a filler, characterized in 15 that the carbon black has a dibutyl phthalate (DBP) absorption number of 40-180 cm³/100 g, a nitrogen adsorption specific surface area (N₂SA) of 40-300 m²/g, a tint strength (TINT) of 50-150% and a light transmittance of toluene extract of not less than 90% and a relation between the nitrogen adsorption specific surface area and the light 20 transmittance of toluene extract satisfies the following equation (I):

$$0.0283 \times A \times (100-B) \leq 40 \dots \dots \text{ (I)}$$

(wherein A is a nitrogen adsorption specific surface area and B is a light transmittance of toluene extract).

[0007] In a preferable embodiment of the rubber composition 25 according to the invention, the relation between the nitrogen adsorption specific surface area and the light transmittance of toluene extract satisfies the following equation (II):

$$0.0283 \times A \times (100-B) \leq 20 \dots \dots \text{ (II)}$$

(wherein A and B are the same as mentioned above).

30 [0008] At this moment, it is further preferable that the relation between the nitrogen adsorption specific surface area and the light transmittance of toluene extract satisfies the following equation (III):

$$0.0283 \times A \times (100-B) \leq 8 \dots \dots \text{ (III)}$$

(wherein A and B are the same as mentioned above).

[0009] In another preferable embodiment of the rubber composition according to the invention, the carbon black has a maximum ultraviolet (UV) absorbance at 330-340 nm of not more than 0.020 and a maximum 5 ultraviolet (UV) absorbance at 260-280 nm of not more than 0.020.

[0010] In the other preferable embodiment of the rubber composition according to the invention, the carbon black has a weight reduction ratio at 400-530°C of not more than 0.20%.

10 [0011] In a further preferable embodiment of the rubber composition according to the invention, the carbon black has an extraction ratio with dichloromethane of not more than 0.12%.

15 [0012] In a still further preferable embodiment of the rubber composition according to the invention, the carbon black has a hydrogen emitting ratio at 2000°C of not less than 0.15%. At this moment, the carbon black is preferable to have a hydrogen emitting ratio at 2000°C of not less than 0.18%, more preferably not less than 0.23%.

[0013] Further, the tire according to the invention is characterized by using the above rubber composition in a tread.

BEST MODE FOR CARRYING OUT THE INVENTION

20 [0014] The invention will be described in detail below. The rubber composition according to the invention comprises 20-250 parts by mass of a carbon black as a filler based on 100 parts by mass of a diene polymer, in which the carbon black has a dibutyl phthalate (DBP) absorption number of 40-180 cm³/100 g, a nitrogen adsorption specific 25 surface area (N₂SA) of 40-300 m²/g, a tint strength (TINT) of 50-150% and a light transmittance of toluene extract of not less than 90% and a relation between the nitrogen adsorption specific surface area and the light transmittance of toluene extract satisfies the above equation (I). In this carbon black, the DBP absorption number, N₂SA and TINT 30 satisfy the above ranges and the light transmittance of toluene extract is not less than 90%, so that the tar component existing on the surface is sufficiently small and the composite between the carbon black and the rubber component is efficiently caused, whereby the wear resistance

of the rubber composition can be considerably improved, and at the same time, the heat buildup of the rubber composition can be lowered.

[0015] The carbon black used in the rubber composition according to the invention is preferable to have a dibutyl phthalate (DBP)

5 absorption number of 40-180 cm³/100 g, preferably 70-170 cm³/100 g.

When the DBP absorption number of the carbon black is less than 40 cm³/100 g, the minimum tensile stress required as a rubber composition for the tire can not be developed, while when it exceeds 180 cm³/100 g, a minimum elongation required can not be ensured.

10 [0016] The carbon black used in the rubber composition according to the invention has a nitrogen adsorption specific surface area (N₂SA) of 40-300 m²/g, preferably 70-250 m²/g, more preferably 70-170 m²/g.

When the nitrogen adsorption specific surface area of the carbon black is less than 40 m²/g, the minimum strength (tensile strength) required 15 as a rubber composition for the tire can not be developed, while when it exceeds 300 m²/g, the dispersibility in the rubber composition can not be sufficiently ensured and hence the wear resistance and the like of the rubber composition are deteriorated.

[0017] The carbon black used in the rubber composition according

20 to the invention has a tint strength (TINT) of 50-150%, preferably 90-145%. When the tint strength of the carbon black is less than 50%, the strength and wear resistance durable in the tire when the rubber composition is applied to the tread can not be developed, while when it exceeds 150%, the viscosity of rubber remarkably rises and it is

25 difficult to provide the rubber composition.

[0018] The carbon black used in the rubber composition according to the invention has a light transmittance of toluene extract of not less than 90%, preferably not less than 95%. When the light transmittance of toluene extract in the carbon black is less than 90%, the tar

30 component existing on the surface of the carbon black, particularly aromatic component becomes large, and hence the rubber composition can not be sufficiently reinforced and the wear resistance and the like of the rubber composition lower.

- [0019] As to the carbon black used in the rubber composition according to the invention, the nitrogen adsorption specific surface area and the light transmittance of toluene extract satisfy the relation of the equation (I), preferably the relation of the equation (II), more 5 preferably the relation of the equation (III) as an absolute value. When a left side in the equations (I), (II) and (III) exceeds 40, the tar component becomes large on the surface of the carbon black, and hence the rubber composition can not be sufficiently reinforced and the wear resistance lowers.
- 10 [0020] The carbon black used in the rubber composition according to the invention is preferable to have a maximum ultraviolet (UV) absorbance at 330-340 nm of not more than 0.020 and a maximum ultraviolet (UV) absorbance at 260-280 nm of not more than 0.020. As the maximum UV absorbances at 330-340 nm and 260-280 nm 15 become small, the aromatic component existing on the surface of the carbon black become less. Therefore, by using the carbon black having the maximum UV absorbances at 330-340 nm and 260-280 nm of not more than 0.020 can be given a high reinforcing property to the rubber composition to thereby improve the wear resistance and the like.
- 20 [0021] The carbon black used in the rubber composition according to the invention is preferable to have a weight reduction ratio at 400-530°C of not more than 0.20%. As the weight reduction ratio at 400-530°C becomes small, the aromatic component existing on the surface of the carbon black become less. Therefore, by using the 25 carbon black having the weight reduction ratio at 400-530°C of not more than 0.20% can be given a high reinforcing property to the rubber composition to thereby improve the wear resistance and the like.
- [0022] The carbon black used in the rubber composition according to the invention is preferable to have an extraction ratio with dichloromethane of not more than 0.12%. As the extraction ratio with dichloromethane becomes small, the aromatic component existing on the surface of the carbon black become less. Therefore, by using the 30 carbon black having the extraction ratio with dichloromethane of not

more than 0.12% can be given a high reinforcing property to the rubber composition to thereby improve the wear resistance and the like.

[0023] As to the carbon black used in the rubber composition according to the invention, the hydrogen emitting ratio at 2000°C is 5 preferably not less than 0.15%, more preferably not less than 0.18%, particularly not less than 0.23%. At this moment, the hydrogen emitting ratio at 2000°C means a ratio of hydrogen quantity produced when the carbon black is heated at 2000°C for 15 minutes to the mass of the carbon black. When the carbon black having a hydrogen emitting ratio at 2000°C of less than 0.15% is used in the rubber 10 composition, the wear resistance of the rubber composition lowers, and the heat buildup of the rubber composition undesirably becomes large.

[0024] The rubber composition according to the invention contains 20-250 parts by mass of the carbon black as a filler based on 100 parts 15 by mass of the diene polymer as a rubber component. When the amount of the carbon black is less than 20 parts by mass, the rigidity of the rubber is low and the wear resistance is insufficient, while when it exceeds 250 parts by mass, the rubber composition becomes too hard, and the wear resistance rather lowers and further the processability of 20 the rubber composition is extremely deteriorated.

[0025] As the diene polymer used as a rubber component in the rubber composition according to the invention are mentioned natural rubber (NR), styrene-butadiene copolymer rubber (SBR), styrene-isoprene copolymer rubber (SIR), polyisoprene rubber (IR), poly-butadiene rubber (BR) and the like. They may be used alone or in a 25 combination of two or more.

[0026] In addition to the above carbon black and the diene polymer, the rubber composition may be properly compounded with additives usually used in the rubber industry such as a filler other than carbon 30 black, a vulcanizing agent, a vulcanization accelerator, an antioxidant, a scorch retarder, a softening agent, zinc oxide, stearic acid, a silane coupling agent and the like within a scope not damaging the object of the invention. As these additives can be preferably used commercially

available ones. Moreover, the rubber composition can be produced by compounding the diene polymer with the carbon black and, if necessary, various additives properly selected, and milling them and warming up and extruding and the like.

- 5 [0027] The tire according to the invention is characterized by using the above rubber composition in the tread. Since the rubber composition is excellent in the wear resistance and low heat buildup, the tire according to the invention is excellent in the wear resistance and low fuel consumption.
- 10 [0028] The following examples are given in illustration of the invention and are not intended as limitations thereof.

[0029] <Examples>

(Production method of carbon black)

In a furnace for the production of carbon black are produced
15 carbon blacks having various properties by properly adjusting an air-introducing condition, a starting oil-introducing condition, and a position and an amount of water introduced for the stop of the reaction and a subsequent temperature, and if necessary, introducing a compound such as water, air or the like into the furnace at a
20 subsequent step. Furthermore, the carbon blacks having various properties are obtained by properly adjusting a drying temperature (150-250°C) of the carbon black after the granulation, if necessary.

[0030] With respect to the thus obtained carbon blacks, the dibutyl phthalate (DBP) absorption number according to ASTM D2414-88 (JIS
25 K6217-97), nitrogen adsorption specific surface area (N₂SA) according to ASTM D3037-88, tint strength (TINT) according to ASTM D3265-88 and light transmittance of toluene extract according to JIS K6218-97 are measured, respectively, and further the UV absorbance, weight reduction ratio, extraction ratio with dichloromethane and hydrogen
30 emitting ratio at 2000°C are measured by the following methods.

The results are shown in Tables 2 and 3.

[0031] (1) UV absorbance

① A carbon black sample is dried in an isothermal drier at 105°C for

1 hour and cooled to room temperature in a desiccator.

② 3.00 g of the sample is weight in an Erienmeyer flask of 100 mL with a co-plug.

5 ③ To the flask is added 30 mL of cyclohexane, which is plugged and violently oscillated for 60 seconds and then left to stand at room temperature for 6 hours.

④ The mixed solution is filtered through a filtrating paper dried at 105°C, and a filtrate is placed into a quartz cell for the UV measurement.

10 ⑤ A solution obtained by carrying out the above operations ③-④ without using the carbon black sample is placed into two quartz cells for the UV measurement, and one of these cells is set to a reference-side light path of a UV measuring device and the other is set to a sample-side light path, and they are adjusted (corrected) at 0-100%.

15 ⑥ With respect to the filtrate obtained in the item ④, maximum light absorbance at 330-340 nm and 260-280 nm are measured.

[0032] (2) Weight reduction ratio

① A carbon black sample is dried in an isothermal drier at 105°C for 1 hour and cooled to room temperature in a desiccator.

20 ② About 10 mg of the sample is weighed on a metal pan for the TGA measurement and subjected to TGA (thermal weight analysis) under a stream of nitrogen gas.

③ The temperature of the sample is raised from 40°C to 600°C at a rate of 10°C/min to measure a weight reduction ratio from 400°C to 530°C based on the initial weight ②.

25 [0033] (3) Extraction ratio with dichloromethane

① About 15 g of a carbon black sample is weighed and placed in a cylindrical filtering paper.

② It is refluxed by heating in a Soxhlet extractor using dichloromethane as an extraction solvent for 30 hours.

30 ③ The extract is dried through evaporation to measure a mass of the residue to thereby determine a mass percentage (ratio of component extracted with dichloromethane).

- [0034] (4) Hydrogen emitting ratio at 2000°C
- ① A carbon black sample is dried in an isothermal drier at 105°C for 1 hour and cooled to room temperature in a desiccator.
- ② About 10 g of the sample is weighed in a tubular vessel made of tin, which is closed by pressing.
- ③ An amount of hydrogen produced when it is heated in a hydrogen analyzing device (EMGA621W, made by Horiba Seisakusho) at 2000°C under a steam of argon gas for 15 minutes is measured to determine a mass percentage.
- 10 [0035] A rubber composition using the above carbon black according to a compounding recipe shown in Table 1 (amount of sulfur compounded is shown in Table 2) is milled in a Banbury mixer and further vulcanized in a pressure type vulcanizing apparatus at 145°C for 30 minutes to obtain a vulcanized rubber. With respect to the resulting vulcanized rubber, the hardness according to JIS K6253-1997, the elongation at break, tensile strength and tensile stress at 300% elongation according to JIS K6251-1993 and the rebound resilience according to JIS K6255-1996 are measured, respectively, and further the wear resistance is evaluated by the following method. These results are shown in Tables 2 and 3. Moreover, the rebound resilience is represented by an index on the basis that the rebound resilience of a test specimen as a standard for comparison is 100, in which the larger the index value, the higher the rebound resilience and the better the low heat buildup.
- 20 [0036] (5) Wear resistance of vulcanized rubber
- A wear loss quantity is measured by using a Lambourn abrasion tester and then an index of wear resistance is calculated according to the following equation. Moreover, the larger the index value, the better the wear resistance.
- 30 Equation: index of wear resistance = wear loss quantity of a test specimen as a standard for comparison/wear loss quantity of each rubber test specimen × 100
- [0037] Furthermore, tires for truck and tires for passenger car are

prepared by applying the rubber composition to a tread, and the wear resistance and heat buildup thereof are evaluated by the following methods. These results are shown in Tables 2 and 3.

[0038] (6) Wear resistance of tire

5 After the tire is mounted onto a truck or a passenger car and run over a distance of 20000 km for the passenger car tire or 4000 km for the truck tire, a residual amount of the groove, and the wear resistance is represented by an index on the basis that a reciprocal of the residual amount of the groove in the tire as a standard for the comparison is

10 100. The larger the index value, the better the wear resistance.

[0039] (7) Heat buildup of tire

After the tire is rotated on a steel drum under a constant load for a constant time, a temperature of a tire tread portion is measured, and the heat buildup is represented by an index on the basis that a reciprocal of the temperature in the tread portion of the tire as a standard for the comparison is 100. The larger the index value, the better the low heat buildup.

[0040] Table 1

	For passenger car	For truck
Compounding recipe of rubber composition	NR (RSS#3)	-
	cis-BR *1	-
	SBR *2	100
	Carbon black	50
	Aromatic oil *3	10
	Antioxidant 6PPD *4	1
	Stearic acid	2
	Zinc oxide	2.5
	Vulcanization accelerator BBS *5	0.6
	Vulcanization accelerator DPG *6	0.6
Tire size		185/60R14
		11.0R22.5

[0041] In Table 1, *1 is BR01 made by JSR Corporation, *2 is #1500 made by JSR Corporation, *3 is AH-58 made by Idemitsu Kosan Co., Ltd., *4 is N-(1,3-dimethylbutyl)-N'-phenyl-p-phenylene diamine, *5 is N-t-butyl-2-benzothiazole sulfenamide, *6 is diphenyl guanidine 5 and *7 is dibenzothiazyl disulfide.

[0042] Table 2(a)

	Air introducing conditions	total amount of air introduced preheating temperature	(kg/h) (°C)	Example 1 1490	Example 2 1488	Example 3 1493	Example 4 1485	Example 5 1490	Example 6 1493
Production conditions of carbon black	Raw oil amount introduced	amount of fuel introduced	(kg/h)	600	603	605	602	600	602
	introducing conditions	amount introduced	(kg/h)	75	74	75	73	75	75
Cooling medium introducing conditions	preheating temperature residual time	amount of cooling water at first stage (milli second)	(°C)	355	352	357	365	355	354
Drying temperature of carbon black	amount of cooling water at second stage (L/h)	(L/h)	(milli second)	190	195	197	187	198	195
DBP absorption number	N ₂ SA (BET surface area)	(cm ³ /100 g)	(m ² /g)	291	295	289	427	305	304
TINT		(%)	(%)	141	145	143	-	-	130
Properties of carbon black	Light transmittance of toluene extract 0.0283 × A × (100-B)	(%)	-	128	128	127	128	126	126
	UV absorbance (330-340 nm)	(%)	131	131	130	130	132	132	132
	UV absorbance (270-280 nm)	(%)	132	132	132	132	133	133	133
	Weight reduction ratio (400-530°C)	(%)	99.2	98.8	99.1	99.2	96.1	95.8	
	Extraction ratio with dichloromethane	(%)	<0.001	<0.001	<0.001	0.001	0.005	0.030	
	Hydrogen emitting ratio (2000°C)	(%)	0.01	0.01	0.01	0.01	0.11	0.11	
	Compounding recipe and tire size	(%)	0.25	0.22	0.16	0.14	0.17	0.17	
	Amount of sulfur compounded *2-1	(part by mass)	1.5	1.5	1.5	1.5	1.5	1.5	1.5
Properties of vulcanized rubber	Hardness	-	67	67	66	67	67	67	67
	Elongation at break	(%)	560	560	570	580	580	580	580
	Tensile strength	(MPa)	31.0	30.8	30.4	30.0	29.1	28.8	
Evaluation	Tensile stress at 300% elongation	(MPa)	14.4	14.2	14.1	13.7	14.7	14.5	
	Lambourn wear resistance	(index)	128	122	117	108	113	109	
	Rebound resilience	(index)	108	107	105	103	105	105	
	Wear resistance of tire	(index)	122	118	114	-	-	-	
	Heart buildup of tire	(index)	107	106	106	-	-	-	

*2-1 amount of sulfur compounded per 100 parts by mass of rubber component

[0042] Table 2(b)

		Example 7	Example 8	Example 9	Example 10	Example 11	Example 12
Air introducing preheating temperature conditions	total amount of air introduced (kg/h) (°C)	1495	1495	1500	1502	1500	1490
Production conditions of carbon black	amount of fuel introduced (kg/h)	605	603	605	607	605	605
Raw oil amount introduced	(kg/h)	75	75	77	77	77	75
Raw oil amount introduced preheating temperature	(kg/h)	360	350	363	362	360	345
Cooling medium introducing conditions	residual time (milli second)	193	198	196	195	198	190
Drying temperature of carbon black	amount of cooling water at first stage (L/h)	5.7	7.1	5.7	5.7	5.7	3.7
DBP absorption number	amount of cooling water at second stage (L/h)	421	332	425	423	428	385
N ₂ SA (BET surface area)	amount of cooling water at second stage (L/h)	-	113	-	-	-	102
TINT	amount of cooling water at second stage (L/h)	192	197	255	195	235	201
Properties of carbon black	DBP absorption number (cm ³ /100 g)	126	126	126	126	126	126
UV absorbance (330-340 nm)	N ₂ SA (BET surface area) (m ² /g)	132	132	132	132	132	129
UV absorbance (270-280 nm)	TINT (%)	133	133	133	133	133	130
Weight reduction ratio (400-530°C)	Light transmittance of toluene extract (%)	95.5	93.2	93.5	92.7	92.8	90.5
Extraction ratio with dichloromethane	0.0283 × A × (100-B)	-	16.8	25.4	24.3	27.3	26.9
Hydrogen emitting ratio (2000°C)	UV absorbance (330-340 nm) (%)	0.005	0.011	0.010	0.015	0.016	0.016
Compounding recipe and tire size	UV absorbance (270-280 nm) (%)	0.005	0.012	0.012	0.016	0.017	0.017
Amount of sulfur compounded *2-1	Weight reduction ratio (400-530°C) (%)	0.11	0.18	0.23	0.18	0.18	0.22
Properties of vulcanized rubber	Extraction ratio with dichloromethane (%)	0.05	0.05	0.05	0.13	0.05	0.11
Evaluation	Hydrogen emitting ratio (2000°C) (%)	0.13	0.16	0.16	0.16	0.17	0.23
	for truck						
Hardness	(part by mass)	1.6	1.6	1.6	1.6	1.6	1.4
Elongation at break	- (%)	67	67	67	67	67	68
Tensile strength	(MPa)	560	560	550	550	540	550
Tensile stress at 300% elongation	(MPa)	28.6	29.0	28.6	28.5	28.0	29.1
Lambourn wear resistance	(index)	14.6	14.8	14.8	14.8	14.8	14.8
Rebound resilience	(index)	106	111	105	106	109	110
Wear resistance of tire	(index)	-	-	-	-	-	-
Heart buildup of tire	(index)	-	-	-	-	-	-

*2-1 amount of sulfur compounded per 100 parts by mass of rubber component

[0043] Table 3

		Comparative Example 1	Comparative Example 2	Comparative Example 3	Comparative Example 4	Comparative Example 5	Comparative Example 13	Comparative Example 14	Comparative Example 6	
Air introducing conditions	total amount of air introduced	(kg/h)	1490	1500	1510	1498	1492	1488	1100	1150
Production conditions	preheating temperature	(°C)	600	602	604	608	603	602	598	597
Raw oil amount introduced	amount of fuel introduced	(kg/h)	75	77	78	75	75	74	50	52
Production conditions of carbon black	preheating temperature	(kg/h)	355	352	350	345	365	342	380	370
Cooling medium introducing conditions	residual time	(°C)	190	195	196	197	196	198	185	187
Drying temperature of carbon black	amount of cooling water at first stage	(millisecond)	3.7	3.7	2.7	1.8	4.7	0.77	78	41
Drying temperature of carbon black	amount of cooling water at second stage	(L/h)	496	498	502	498	281	486	376	380
DBP absorption number	N ₂ SA (BET surface area)	(cm ³ /100 g)	127	127	129	127	125	126	114	112
TINT		(m ² /g)	129	130	132	130	126	124	71	73
Properties of carbon black	Light transmittance of toluene extract	(%)	88	86.9	65	40	98	55	99	50
	0.0283 × A × (100-B)	-	43.8	51.5	130.7	220.7	7.1	157.9	2.0	103.3
UV absorbance (330-340 nm)	UV absorbance (270-280 nm)	(%)	0.080	0.130	0.180	0.220	0.005	0.190	0.002	0.210
Weight reduction ratio (400-530°C)		(%)	0.100	0.140	0.190	0.250	0.006	0.210	0.003	0.230
Extraction ratio with dichloromethane		(%)	0.22	0.21	0.38	0.42	0.05	0.32	0.08	0.34
Hydrogen emitting ratio (2000°C)		(%)	0.10	0.13	0.22	0.28	0.10	0.22	0.11	0.25
Compounding recipe and tire size	Amount of sulfur compounded *3-1	(%)	0.17	0.17	0.22	0.28	0.18	0.27	0.24	0.28
Evaluation	Hardness	(part by mass)	1.5	1.5	1.4	1.3	1.5	1.4	1.5	1.4
Properties of vulcanized rubber	Elongation at break	-	66	64	67	67	63	62	58	57
	Tensile strength	(%)	520	480	450	430	550	460	580	510
	Tensile stress at 300% elongation	(MPa)	26.2	25.6	22.9	21.2	29.1	27.0	23.2	20.8
	Lambourn wear resistance	(MPa)	14.4	13.8	14.7	14.6	13.6	13.2	12.1	12.1
	Rebound resilience	(index)	101	100	90	79	114	100	116	100
	Wear resistance of tire	(index)	98	100	92	86	106	100	107	100
	Heart buildup of tire	(index)	-	100	-	-	106	100	109	100
			-	-	-	-	105	100	107	100

for passenger car
for truck

[0044] In Tables 2 and 3, Examples 1-12 and Comparative Examples 1, 3 and 4 are compared with the vulcanized rubber and tire of Comparative Example 2 as a standard, and Example 13 is compared with the vulcanized rubber and tire of Comparative Example 5 as a

5 standard, and Example 14 is compared with the vulcanized rubber and tire of Comparative Example 6 as a standard.

[0045] As seen from Tables 2 and 3, the vulcanized rubbers of the examples are high in the Lambourn wear resistance and rebound resilience, and the tires using such rubber compositions are excellent
10 in the wear resistance and low heat buildup. On the other hand, the vulcanized rubbers of the comparative examples compounded with the carbon black not satisfying the properties defined in the invention are low in the Lambourn wear resistance and rebound resilience as compared with the vulcanized rubbers of the examples, and the tires of
15 the comparative examples using these rubber compositions are poor in the wear resistance and low heat buildup as compared with the tires of the examples.

INDUSTRIAL APPLICABILITY

[0046] According to the invention, by using a carbon black having
20 particular properties and a small tar component in a rubber composition compounded with the carbon black can be provided a rubber composition having a high strength at break and excellent wear resistance and low heat buildup. Also, there can be provided a tire using such a rubber composition in a tread and having excellent wear
25 resistance and low fuel consumption.